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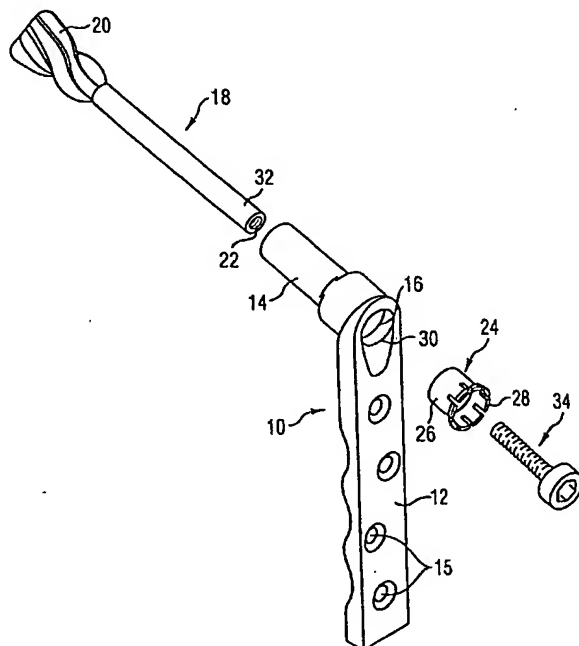
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(54) Title: DEVICE FOR ROTATIONAL STABILIZATION OF BONE SEGMENTS



(57) Abstract: A device for rotational stabilization of bone segments comprising a bone plate (10), a bone lag screw (18), and a locking collar (50). The bone lag screw (18) has a bone-engagement end (20), a distal end, and a keyed cross-sectional profile (32), the bone-engagement end (20) configured for engaging a first bone segment. The bone plate (10) has a flat portion (12) for engaging a second bone segment and a barrel portion (14) having an internal bore for slidably receiving the lag screw (18). The locking collar (50) has a keyed internal profile (21) that mates with the keyed cross-sectional profile (32) of the lag screw (18) to rotationally couple the locking collar (50) and the lag screw (18) when the lag screw (18) is inserted through the locking collar (50), and an outer surface configured and dimensioned for free rotation, in a first position, within the internal bore (16) of the bone plate barrel portion (14) and frictionally engaging, in a second position, the internal bore (16) of the bone plate barrel portion (14) to resist or prevent rotation of the collar (50) relative to the bone plate (10), and thereby resist or prevent rotation of the lag screw (18) relative to the bone plate (10). The frictional engagement is achieved by a deformation of the distal end (56) of the locking collar (50) within the internal bore (16) of the bone plate (10). This deformation is achieved by the application of force to the collar in the proximal direction.

WO 03/028567 A1

WO 03/028567 A1



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**DEVICE FOR ROTATIONAL  
STABILIZATION OF BONE SEGMENTS**

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**RELATED APPLICATIONS**

This application is a continuation-in-part of currently pending United States Patent Application Serial No. 09/542,821, filed April 4, 2000.

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**FIELD OF THE INVENTION**

The present invention relates generally to connection devices, and, more particularly, to a bone connection device for rotational stabilization of bone segments.

**BACKGROUND OF THE INVENTION**

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Devices for the repair of large bone fractures (e.g., fractures of the femoral neck) have generally consisted of some combination of a lag screw with a side plate and some means for attaching these two components to one another and to the fractured bone segments. The ability to rotationally lock a lag screw (also known as a "hip screw") relative to its side plate is very important in such devices because rotational movement of the lag screw relative to the side plate following implantation can cause premature wear of the bone fragment and result in loosening of the system prior to complete healing.

20

Prior art devices have attempted to rotationally lock installed lag screws using keys, pins, rings, splines, etc. *See e.g.*, U.S. Patents 5,007,910 and 5,514,138 to Anapliotis, et al. and McCarthy, respectively. The additional operation time and tools required to align and properly install such equipment has fueled a desire for a simpler and more effective device for aligning and rotationally locking the lag screw relative to the side plate. Such a device would reduce surgical operation time and complexity and provide a more effective and efficient mechanism for rotationally locking a lag screw to its corresponding side plate – an obvious benefit to both orthopaedic physicians and patients.

25  
30**SUMMARY OF THE INVENTION**

In a preferred embodiment, the present invention is a device for rotational stabilization of bone segments comprising: a bone lag screw having a bone-engagement end, a distal end, and a keyed cross-sectional profile, the bone-engagement end configured for engaging a first bone segment; a bone plate having a flat portion for engaging a second bone

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segment and a barrel portion having an internal bore for slidably receiving the lag screw;  
and a locking collar having a keyed internal profile that mates with the keyed cross-sectional  
profile of the lag screw to rotationally couple the locking collar and the lag screw when the  
lag screw is inserted through the locking collar, and an outer surface configured and  
5 dimensioned for (1) free rotation, in a first position, within the internal bore of the bone  
plate barrel portion and (2) frictionally engaging, in a second position, the internal bore of  
the bone plate barrel portion to resist or prevent rotation of the collar relative to the bone  
plate, and thereby resist or prevent rotation of the lag screw relative to the bone plate. The  
locking collar may be cylindrical, and the outer surface of the locking collar may be formed  
10 with a taper. The taper of the outer surface of the locking collar may range from about 0  
degrees to about 10 degrees. The taper of the outer surface of the locking collar may be  
defined by a major diameter and a minor diameter, a distal end of the collar having the  
major diameter, and a proximal end of the collar having the minor diameter.

The internal bore of the bone plate barrel portion may also be formed with a  
15 taper and the taper of the outer surface of the locking collar may be of the same degree and  
profile as the taper of the internal bore of the bone plate barrel portion. In one specific  
example, an impact force on the distal end of the locking collar frictionally locks the tapered  
outer surface of the locking collar to the tapered inner surface of the bone plate internal  
bore, preventing further rotation of the collar relative to the bone plate, and thereby  
20 preventing further rotation of the lag screw relative to the bone plate. This frictional  
locking is known as the Morse Taper effect. The components described above (i.e., lag  
screw, bone plate, locking collar) may be formed of any bio-compatible material, but are  
preferably of stainless steel, titanium alloy, or titanium.

Alternatively, the outer surface of the locking collar may be formed with a  
25 reverse taper defined by a major diameter and a minor diameter, a proximal end of the collar  
having the major diameter, and a distal end of the collar having the minor diameter. The  
locking collar, in the second position, may then be frictionally engaged in a proximal section  
of the internal bore of the bone plate by a force in a distal direction (i.e., a force directed  
away from, rather than toward, the patient's body), such as that applied with a slide-  
30 hammer.

The barrel portion of the bone plate may be angled relative to the flat  
portion, and the device may be configured and adapted for repair of fractures of the femoral  
neck (i.e., hip bone). It should be pointed out, however, that the device is generally  
applicable to any type of bone fracture where rotational stabilization is important. In  
35 addition, the locking collar may be formed with a plurality of partial lengthwise slots

extending from a distal end of the collar toward the proximal end of the collar. The lag screw may be formed with a cancellous screw thread, or it may be formed with a plurality of helically twisted blades.

In one variation of this embodiment, the device may further comprise a  
5 threaded bore in the distal end of the lag screw, and a compression screw insertable into the threaded bore of the lag screw. When threaded into the threaded bore of the lag screw, the compression screw abuts a distal end of the locking collar and draws the lag screw in an axial direction to join the two bone segments and reduce the fracture. As with the elements discussed above, the compression screw may be formed of stainless steel, titanium alloy, or  
10 titanium.

In another embodiment, the invention is a device for rotational stabilization of bone segments comprising: a bone lag screw having a bone-engagement end and a distal end, the bone-engagement end configured for engaging a first bone segment; a bone plate having a flat portion for engaging a second bone segment and a barrel portion having an  
15 internal bore for slidably receiving the lag screw, part of the internal bore having a taper; and a cylindrical locking collar having a hollowed cylindrical interior, a keyed internal profile that mates with the keyed cross-sectional profile of the lag screw to rotationally couple the locking collar and the lag screw when the lag screw is inserted through the locking collar, and a tapered outer surface configured and dimensioned for (1) free rotation,  
20 in a first position, within the internal bore of the bone plate barrel portion and (2) frictionally engaging, in a second position, the internal bore of the bone plate barrel portion to resist or prevent rotation of the collar relative to the bone plate, and thereby resist or prevent rotation of the lag screw relative to the bone plate. An impact force on the distal end of the locking collar frictionally locks the tapered outer surface of the locking collar to  
25 the tapered inner surface of the bone plate internal bore, preventing further rotation of the collar relative to the bone plate, and thereby preventing further rotation of the lag screw relative to the bone plate. This frictional locking is known as the Morse Taper effect. The taper of the outer surface of the locking collar may range from about 0 degrees to about 10 degrees, and may be defined by a major diameter and a minor diameter, a distal end of the  
30 collar having the major diameter, and a proximal end of the collar having the minor diameter. The barrel portion of the bone plate may be angled relative to the flat portion, and the device may be configured and adapted for repair of fractures of the femoral neck (i.e., hip bone), but is generally applicable to any type of bone fracture where rotational stabilization is important. The components described above (i.e., lag screw, bone plate,  
35 locking collar) may be formed of any biocompatible material, but are preferably formed of

stainless steel, titanium alloy, or titanium. In addition, the locking collar may be formed with a plurality of partial lengthwise slots extending from the distal end of the collar toward the proximal end of the collar. The taper of the outer surface of the locking collar may be of the same degree and profile as the taper of the internal bore of the angled barrel portion.

5           In an alternative arrangement, the outer surface of the locking collar may be formed with a reverse taper defined by a major diameter and a minor diameter, a proximal end of the collar having the major diameter, and a distal end of the collar having the minor diameter. The locking collar, in the second position, may then be frictionally engaged in a proximal section of the internal bore of the bone plate by a force in a distal direction (i.e., a  
10           force directed away from, rather than toward, the patient's body), such as that applied with a slap-hammer.

          The device may further comprise a threaded bore in the distal end of the lag screw, and a compression screw insertable into the threaded bore of the lag screw. When threaded into the threaded bore of the lag screw, the compression screw abuts the distal end  
15           of the locking collar and draws the lag screw in an axial direction to join the two bone segments and reduce the fracture. As with the elements discussed above, the compression screw may be formed of stainless steel, titanium alloy, or titanium.

          In still another preferred embodiment, the invention is a device for rotational stabilization of bone segments comprising a bone lag screw having a bone-engagement end, a distal end, and a keyed cross-sectional profile, the bone-engagement end configured for  
20           engaging a first bone segment; a bone plate having a flat portion for engaging a second bone segment and a barrel portion having an internal bore for slidably receiving the lag screw; and a locking collar having a proximal end, a distal end, a keyed internal profile and a deformable portion at the distal end; wherein the keyed internal profile mates with the keyed  
25           cross-sectional profile of the lag screw to rotationally couple the locking collar and the lag screw when the lag screw is inserted through the locking collar, and the deformable portion is configured and dimensioned for (1) free rotation, in a first position, within the internal bore of the bone plate barrel portion and (2) frictionally engaging, in a second position, the  
30           internal bore of the bone plate barrel portion to resist or prevent rotation of the collar relative to the bone plate, and thereby resist or prevent rotation of the lag screw relative to the bone plate. An axial impact force in the proximal direction on the distal end of the  
locking collar frictionally locks the deformable portion of the locking collar to the inner  
surface of the bone plate internal bore, preventing further rotation of the collar relative to  
the bone plate, and thereby preventing further rotation of the lag screw relative to the bone  
35           plate. The locking collar may be substantially cylindrical, and the deformable portion of the

locking collar may have a maximum diameter at the distal end of the locking collar and taper toward a proximal end of the locking collar, forming an angle of about 20° with a longitudinal axis (about 70° with a vertical axis) of the locking collar. The maximum diameter may be greater than the internal diameter of the internal bore when the locking collar is in the first position. The internal bore of the bone plate barrel portion may have a circumferential groove at a distal end which engages the distal end of the locking collar such that the collar freely rotates within the internal bore of the barrel in the first position. The deformable portion may also include a plurality of deformable tabs extending part of the distance from the distal end of the locking collar toward the proximal end of the locking collar. These deformable tabs, which may be spaced about the circumference of the distal end of the locking collar, may also have flat portions at the distal end of the locking collar and taper toward the proximal end of the locking collar.

The barrel portion of the bone plate may be angled relative to the flat portion, the first bone segment is the femoral head, the second bone segment is the femoral shaft, and the device is configured and adapted for repair of fractures of the femoral neck. As in the previous embodiments, the lag screw may be formed with a cancellous screw thread or a plurality of helically twisted blades, and the lag screw, bone plate, and locking collar may be formed of stainless steel, titanium alloy, or titanium.

The device may further comprise a threaded bore in the distal end of the lag screw, and a compression screw insertable into the threaded bore of the lag screw. When threaded into the threaded bore of the lag screw, the compression screw abuts the distal end of the locking collar and draws the lag screw in an axial direction to join the two bone segments and reduce the fracture. As with the elements discussed above, the compression screw may be formed of stainless steel, titanium alloy, or titanium.

In still another preferred embodiment, the invention provides an improved method for rotationally stabilizing bone segments utilizing a bone lag screw and a bone plate, the improvement comprising: sufficiently locking the bone screw to the bone plate by frictional engagement to rotationally stabilize the bone segments relative to one another. The method may further comprise: inserting a locking collar into a barrel portion of a bone plate; inserting a lag screw through the locking collar and barrel portion; rotationally coupling the locking collar and the lag screw; attaching the bone-engagement end of the lag screw to a first bone segment; and impacting the locking collar to frictionally engage an outer surface of the locking collar to the internal bore to resist or prevent further rotation of the collar relative to the bone plate, and thereby prevent further rotation of the lag screw relative to the bone plate. In one variation, a deformable distal end of the locking collar

frictionally engages the internal bore to resist or prevent further rotation of the collar relative to the bone plate, and thereby prevent further rotation of the lag screw relative to the bone plate.

## 5 BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will be understood and appreciated more fully from the following detailed description, taken in conjunction with the drawings in which:

FIG. 1 is an isometric view of the disassembled components of the device in a preferred embodiment of the present invention;

10 FIG. 2 is a cross-sectional view of the bone plate and locking collar of one preferred embodiment of the present invention;

FIG. 3A is a cross-sectional view of the locking collar shown in FIG. 2;

FIG. 3B is a plan view of the locking collar shown in FIG. 2;

15 FIG. 4 is a cross-sectional view of the bone plate and locking collar of another preferred embodiment of the present invention;

FIG. 5A is a side view of the locking collar shown in FIG. 4;

FIG. 5B is a plan view of the locking collar shown in FIG. 4;

FIG. 5C is a cross-sectional view of the locking collar taken along line 5C-5C shown in FIG. 5B;

20 FIG. 6 is a cross-sectional view through a pair of bone segments demonstrating the application of one embodiment of the device of the present invention; and

FIG. 7 is a cross-sectional view through a pair of bone segments demonstrating the application of another embodiment of the device of the present invention.

## 25 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Reference is now made to FIG. 1, which is an isometric view of the disassembled components of one embodiment of the device of the present invention. The device allows a lag screw (or hip screw) to be aligned and rotationally locked within the bore of a bone repair plate. While the device is described in the context of hip fracture repair, it should be pointed out that the device may also be used in the repair of other bone fractures, such as knee joint fractures.

35 A side plate 10 has a flat portion 12 for attachment to the femur shaft (not shown) and an angled barrel portion 14 having an internal bore 16. The flat portion 12 has holes 15 (which may be self-compressing screw holes) for connection to the femoral shaft using screws or other coupling means. The internal bore 16 is formed with a taper or cone,



as will be explained below with reference to FIG. 2. A lag screw 18 has a drilling portion 20 at a bone-engagement end and a threaded internal bore 22 at a distal end. The lag screw 18 may be formed with a conventional cancellous screw thread 46 (as shown in FIG. 5), or may be formed with a plurality of helically twisted blades (as shown in FIG. 1), for example  
5 such as that disclosed in U.S. Patent No. 5,741,256 to Bresina, incorporated herein by reference. With regard to the descriptions of the elements of the present invention, it should be pointed out that the terms "proximal" and "distal" are defined with relation to the body of the patient (i.e., the person receiving the bone stabilization device). For example, the term "proximal" is used to describe that portion of a given element closer to the center  
10 of the patient's body, and the term "distal" refers to that portion of the element further away from the center of the patient's body.

In one embodiment, a locking collar 24 has a hollow cylindrical interior and an outer surface 26 formed with a taper. The taper of the outer surface 26 of locking collar 24, ranging from about 0 degrees to about 10 degrees, is of the same degree and profile as  
15 the taper of the internal bore 16. The locking collar 24 also has a circumferential lip 28 (see FIG. 3A) at a distal end that mates with a circumferential groove 30 at a distal end of the internal bore 16. When the locking collar 24 is introduced into the internal bore 16, the circumferential lip 28 engages the circumferential groove 30, such that the collar is axially restrained in the bore, but is free to rotate with respect to the bore. It should be noted that  
20 the bone stabilization device may be supplied to physicians with the locking collar already engaged in the circumferential groove 30 of the bone plate internal bore 16. The locking collar also has a keyed internal profile, as will be explained below with reference to FIG. 3B, that mates with a keyed cross-sectional profile 32 on the shaft of the lag screw 18, to rotationally couple the locking collar 24 to the lag screw 18 when the lag screw is inserted  
25 through the internal bore 16 and the locking collar 24. The locking collar 24 also facilitates the proper alignment of the lag screw 18 and side plate 10, while simultaneously permitting the screw 18 to rotate freely so that it can engage the bone segment during installation. This integral alignment function of the locking collar 24 eliminates the need for additional components or alignment tools.

30 After the locking collar 24 is placed within bore 16, and the lag screw 18 is inserted through the collar and has satisfactorily engaged the bone, an impact force is applied to the exposed end of the collar (i.e., the distal end), causing the lip 28 to become disengaged from the groove 30, and driving the collar proximally inward along the bore 16, resulting in the tapered outer surface 26 of the locking collar becoming frictionally locked  
35 with the tapered surface of the internal bore 16. This frictional locking, known as the

Morse Taper effect, prevents further movement (both axial and rotational) of the collar 24 relative to the internal bore 16, and so prevents further rotation of the lag screw 18. This rotational stabilization of the lag screw relative to the bone plate will prevent premature wear of the bone fragments and loosening of the system prior to complete bone healing.

5 It should be noted that in an alternate embodiment, the bore may have a reverse taper, as compared to that of the embodiment illustrated in FIGS. 2, 3A and 3B. In this embodiment, the bore has its major diameter at the proximal end, its minor diameter at the distal end, and the collar 24 is locked in place at the proximal end of the internal bore 16 by a force in the distal direction, such as that applied by a slide-hammer.

10 At this point, the lag screw is rotationally fixed relative to the side plate 10 and locking collar 24, but the lag screw may still slide axially relative to the collar and side plate. A compression screw 34 may be inserted into the threaded bore 22 of the lag screw, abutting the distal end of the locking collar 24 and drawing the lag screw axially in the distal direction, to join the separated bone segments (i.e., reducing the fracture) and promote the  
15 desired healing. The elements described above may be formed of stainless steel, titanium alloy, titanium, or any other material with suitable strength and bio-compatibility.

As described below and shown in FIGS. 4, 5A, 5B and 5C, in another preferred embodiment, a locking collar 50 has a deformable portion 52. Upon application of an impact force to the exposed distal end of collar 50, collar 50 is driven proximally  
20 inward along bore 16 and deformable portion 52 becomes frictionally locked within internal bore 16.

Reference is now made to FIG. 2, which is a cross-sectional view of the side plate and locking collar of one preferred embodiment of the present invention. As discussed above, the side plate 10 has a flat portion 12 for connection to the femoral shaft and an  
25 angled barrel portion 14 having an internal bore 16 for slidably receiving a lag screw (not shown). The bore 16 has a tapered surface 17 along part of its length. A locking collar 24 sits within the internal bore 16, a circumferential lip 28 on the collar 24 rotatably engaging a circumferential groove 30 on the bore 16. The collar 24 has a tapered outer surface 26, with the same degree and profile as the tapered surface 17 of internal bore 16. Prior to  
30 insertion and alignment of the lag screw (not shown) and application of an impact force to the distal end 19 of the collar, the collar can rotatably slide within the bore 16. The collar 24 has a keyed internal profile 21, as shown most clearly in FIG. 3B, for mating and rotationally coupling with a corresponding keyed cross-sectional profile of the lag screw. Thus, upon insertion of the lag screw through the bore 16 and collar 24, rotation of the lag  
35 screw causes rotation of the locking collar 24 relative to the bore 16. Upon application of

an impact force to distal end 19 of the collar, the tapered outer surface 26 of the collar becomes frictionally locked with tapered surface 17 of bore 16. As described above, this is known as the Morse Taper effect.

Reference is now made to FIGS. 3A and 3B, which are sectional and plan views, respectively, of the locking collar of one preferred embodiment of the present invention. Locking collar 24 has a tapered outer surface 26, with a distal end 19, having the major diameter, and a proximal end 23, having the minor diameter. The distal end comprises a flat outer face designed to correspond to the flat underside of the head of a compression screw (not shown). A circumferential lip 28 is provided at distal end 19 for engaging a groove on the internal bore of the side plate (see FIGS. 1 and 2). Collar 24 also has a keyed internal profile 21, for mating with a corresponding keyed cross-sectional profile on the lag screw (not shown), and a plurality of lengthwise slots 27 extending from the distal end 19 toward the proximal end 23. These slots 27 facilitate disengagement of the circumferential lip 28 from the circumferential groove on the internal bore of the side plate (not shown), after the lag screw is satisfactorily engaged with the bone. As discussed above, the collar 24 facilitates alignment and ensures proper orientation of the lag screw, while allowing the screw to rotate freely so that its drilling portion 20 can engage its respective bone fragment during installation. An impact force subsequently applied to distal end 19 frictionally locks the tapered outer surface 26 to the mating tapered surface of the side plate internal bore (see FIG. 2). The locking collar may be formed of stainless steel, titanium, titanium alloy or any other material with suitable strength and bio-compatible characteristics.

Reference is now made to FIG. 4, which is a cross-sectional view of the side plate and locking collar of another preferred embodiment of the present invention. As for the embodiment discussed above, the side plate 10 has a flat portion 12 for connection to the femoral shaft and an angled barrel portion 14 having an internal bore 16 for slidably receiving a lag screw (not shown). A locking collar 50 sits within the internal bore 16, and a deformable portion 52 on the collar 50 rotatably engages a circumferential groove 30 on the bore 16. Deformable portion 52 includes a plurality of deformable, lengthwise tabs 54 (shown more clearly in FIGS. 5A-5C discussed below) that extend partially along the axial extent of the deformable portion. These tabs 54 have initial flat portions 55 at the distal end 56 of collar 50 (where the height of tabs 54, as measured radially from the axial centerline of the collar, is greatest) and then taper toward the proximal end 58 of collar 50 (where the height of tabs 54 is smallest), forming an angle of about 20° with a longitudinal axis (70° with a vertical). Flat portions 55 of tabs 54 may have a length of about 1.3 mm. Prior to

insertion and alignment of the lag screw (not shown) and application of an impact force to the distal end 56 of the collar, the collar can rotatably slide within the bore 16. The collar 50 has a keyed internal profile 21, as shown most clearly in FIG. 5B, for mating and rotationally coupling with a corresponding keyed cross-sectional profile of the lag screw.

5 Thus, upon insertion of the lag screw through the bore 16 and collar 50, rotation of the lag screw causes rotation of the locking collar 50 relative to the bore 16. Upon application of an impact force to distal end 56 of collar 50, collar 50 is driven proximally inward along bore 16 causing the high portions of tabs 54 to come into contact with the walls of the internal bore 16. With sufficient impact force, the tabs 54 will deform causing the collar 50  
10 to become frictionally locked (both axially and rotationally) with the internal bore 16.

Reference is now made to FIGS. 5A, 5B and 5C, which are side, plan and sectional views, respectively, of the locking collar 50 of this preferred embodiment of the present invention. Locking collar 50, which is substantially cylindrical, has a deformable portion 52, which includes a plurality of deformable, partial lengthwise tabs 54 having initial  
15 flat portions 55 at the distal end 56 and tapering toward the proximal end 58 of collar 50. As shown in FIG. 5B, tabs 54 are spaced about the circumference of collar 50 at distal end 56. As shown best in FIGS. 5A and 5B, deformable portion 52 has a maximum diameter at the distal end 56 of collar 50. This diameter is greater than the diameter of the internal bore 16 of the bone plate barrel portion (see FIG. 4). Distal end 56 comprises an outer face,  
20 which may be flat or concave, designed to correspond to the underside of the head of a compression screw (not shown). Deformable portion 52 engages a groove 30 on the internal bore of the side plate (see FIG. 4) allowing collar 50 to rotatably slide within the bore 16. Collar 50 also has a keyed internal profile 21, for mating with a corresponding keyed cross-sectional profile on the lag screw (not shown).

25 As discussed above, collar 50 facilitates alignment and ensures proper orientation of the lag screw, while allowing the screw to rotate freely so that its drilling portion 20 can engage its respective bone fragment during installation. An impact force subsequently applied to distal end 56 frictionally locks the deformable tabs 54 of deformable portion 52 to the inner surface of the side plate internal bore (see FIG. 2). This friction, or  
30 interference, fit prevents further rotation of the collar 50 relative to the internal bore. The locking collar 50 may be formed of stainless steel, titanium, titanium alloy or any other material with suitable strength and bio-compatible characteristics.

Reference is now made to FIGS. 6 and 7 which demonstrate the application of the device of the present invention to repair a fracture of the femoral neck (i.e., hip). As  
35 shown, the assembled device 40 is used to join two bone segments 41, 42 (i.e., the femoral

head and the femoral shaft). A lag screw 18 having a bone-engagement end, a distal end, and a keyed cross-sectional profile over part of its length is provided. The bone-engagement end of lag screw 18, which may have a plurality of helically twisted blades 45 (shown in FIG. 6) or a cancellous screw thread 46 (shown in FIG. 7), is configured for engaging first bone segment 41 and the distal end has a threaded bore.

A side plate 10 is provided having a flat portion for engaging second bone segment 42 and an angled barrel portion 14 with an internal bore for slidably receiving the lag screw. A portion of the internal bore (not shown) has a taper and a distal end of the internal bore has a circumferential groove.

A cylindrical locking collar 24 or 50 (not shown) having a hollowed cylindrical interior and a keyed internal profile is also provided. In one embodiment, the collar has an outer surface formed with a taper defined by a major diameter and a minor diameter, a distal end of the collar having the major diameter, a proximal end of the collar having the minor diameter, and a circumferential lip at the distal end for engaging the circumferential groove of the internal bore. In another embodiment, the collar has a deformable portion with a maximum diameter greater than the diameter of the internal bore, where the distal end of the locking collar also engages a circumferential groove of the internal bore.

The system is assembled by inserting the cylindrical locking collar into the internal bore of the bone plate so that it rotatably engages the internal bore. As discussed above, the system may be supplied to physicians with the locking collar already engaged in the internal bore of the bone plate, thus eliminating the need for physicians or technicians to insert the collar into the bore of the bone plate. The lag screw 18 is inserted into the locking collar, such that the keyed cross-sectional profile of the lag screw mates with the keyed internal profile of the locking collar to rotationally couple the locking collar and the lag screw. After proper engagement of the lag screw 34 with the first bone segment 41, the distal end of the locking collar (not shown) is impacted using a mallet-type instrument, frictionally locking the collar within the angled barrel portion 14 of the side plate 10. This frictional locking prevents further rotation of the collar relative to the bone plate, and thereby prevents further rotation of the lag screw relative to the bone plate. In an alternative arrangement, the collar is locked in place by a force in the distal direction, such as that applied by a slap-hammer. The side plate 10 would typically be anchored to the femoral shaft 42 using bone screws 44 (formed of stainless steel, titanium or titanium alloy). A compression screw 34 would then be inserted into the threaded bore (see FIG. 1) of the lag screw, abutting the locking collar and axially drawing bone segment 41 toward bone

segment 42 (see FIGS. 6 & 7). Alternatively, the side plate 10 may be affixed to the femoral shaft prior to impact of the locking collar.

While the present invention has been described with reference to the preferred embodiments, those skilled in the art will recognize that numerous variations and modifications may be made without departing from the scope of the present invention. This is especially true with regard to the shape and configuration of the bone plate and lag screw, which can be adjusted according to the type and location of the bone segments to be joined. Accordingly, it should be clearly understood that the embodiments of the invention described above are not intended as limitations on the scope of the invention, which is defined only by the following claims.

What is claimed is:

- 35

6. The device of claim 5, wherein the locking collar has a longitudinal axis and the tapered, deformable portion forms an angle of about 20° with the longitudinal axis.

7. The device of claim 6, wherein the deformable portion includes a plurality of  
5 deformable tabs extending part of the distance from the distal end of the locking collar toward the proximal end of the locking collar.

8. The device of claim 7, wherein the deformable tabs have flat portions at the distal end of the locking collar and taper toward the proximal end of the locking collar.

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9. The device of claim 7, wherein the distal end of the locking collar has a circumference, and the plurality of deformable tabs are spaced about the circumference.

10. The device of claim 7, wherein the locking collar, in the second position, is  
15 frictionally engaged in the internal bore of the bone plate by deformation of the deformable tabs.

11. The device of claim 4, wherein the internal bore of the bone plate barrel  
portion has a diameter, and the maximum diameter of the deformable portion, when the  
20 collar is in the first position, is greater than the diameter of the internal bore.

12. The device of claim 1, wherein the locking collar is substantially cylindrical.

13. The device of claim 1, wherein the barrel portion of the bone plate is angled  
25 relative to the flat portion, the first bone segment is the femoral head, the second bone segment is the femoral shaft, and the device is configured and adapted for repair of fractures of the femoral neck.

14. The device of claim 1, wherein the lag screw is formed with a cancellous  
30 screw thread.

15. The device of claim 1, wherein the lag screw is formed with a plurality of helically twisted blades.

16. The device of claim 1, wherein the lag screw, bone plate, and locking collar  
35 are formed of stainless steel, titanium alloy, or titanium.



17. The device of claim 1, further comprising:  
a threaded bore in the distal end of the lag screw; and  
a compression screw insertable into the threaded bore of the lag screw.
- 5 18. The device of claim 17, wherein the compression screw, when threaded into the threaded bore of the lag screw, abuts a distal end of the locking collar and draws the lag screw in an axial direction to join the two bone segments.
- 10 19. The device of claim 17, wherein the compression screw is formed of stainless steel, titanium alloy, or titanium.
- 15 20. A device for rotational stabilization of bone segments comprising:  
a bone lag screw having a bone-engagement end, a distal end, and a keyed cross-sectional profile, the bone-engagement end configured for engaging a first bone segment;  
a bone plate having a flat portion for engaging a second bone segment and a barrel portion having an internal bore for slidably receiving the lag screw; and  
20 a substantially cylindrical locking collar having a proximal end, a distal end, a hollowed cylindrical interior, a keyed internal profile and a plurality of deformable tabs at the distal end;  
wherein the keyed internal profile mates with the keyed cross-sectional profile of the lag screw to rotationally couple the locking collar and the lag screw when the lag screw is inserted through the locking collar, and the locking collar is configured and dimensioned for  
25 (1) free rotation, in a first position, within the internal bore of the bone plate barrel portion and (2) frictionally engaging, in a second position, the internal bore of the bone plate barrel portion to resist or prevent rotation of the collar relative to the bone plate, and thereby resist or prevent rotation of the lag screw relative to the bone plate.
- 30 21. The device of claim 20, wherein the locking collar has a maximum diameter at its distal end.
- 35 22. The device of claim 21, wherein each of the deformable tabs has a flat portion at the distal end of the locking collar and tapers from the flat portion toward the proximal end of the locking collar.

23. The device of claim 22, wherein the locking collar has a longitudinal axis and the deformable tabs taper at 20° to the longitudinal axis.

24. The device of claim 20, wherein the distal end of the locking collar has a circumference, and the plurality of deformable tabs are spaced about the circumference.

25. The device of claim 21, wherein the internal bore of the bone plate barrel portion has a diameter, and the maximum diameter of the locking collar, when the collar is in the first position, is greater than the diameter of the internal bore.

26. The device of claim 20, wherein the locking collar, in the second position, is frictionally engaged in the internal bore of the bone plate by deformation of the deformable tabs within the internal bore of the bone plate.

27. The device of claim 26, wherein the deformation of the deformable tabs of the locking collar within the internal bore of the bone plate is achieved by application of a force on the locking collar in a proximal direction.

28. The device of claim 20, wherein the barrel portion of the bone plate is angled relative to the flat portion, the first bone segment is the femoral head, the second bone segment is the femoral shaft, and the device is configured and adapted for repair of fractures of the femoral neck.

29. The device of claim 20, wherein the lag screw, bone plate, and locking collar are formed of stainless steel, titanium alloy, or titanium.

30. The device of claim 20, further comprising:  
a threaded bore in the distal end of the lag screw; and  
a compression screw insertable into the threaded bore of the lag screw.

31. The device of claim 30, wherein the compression screw, when threaded into the threaded bore of the lag screw, abuts a distal end of the locking collar and draws the lag screw in an axial direction to join the two bone segments.

32. The device of claim 30, wherein the compression screw is formed of a stainless steel, titanium alloy, or titanium.

33. The device of claim 20, further comprising a circumferential groove at a distal end of the internal bore of the bone plate barrel portion which engages the distal end of the locking collar such that the collar freely rotates within the internal bore of the barrel in the first position.

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1/5

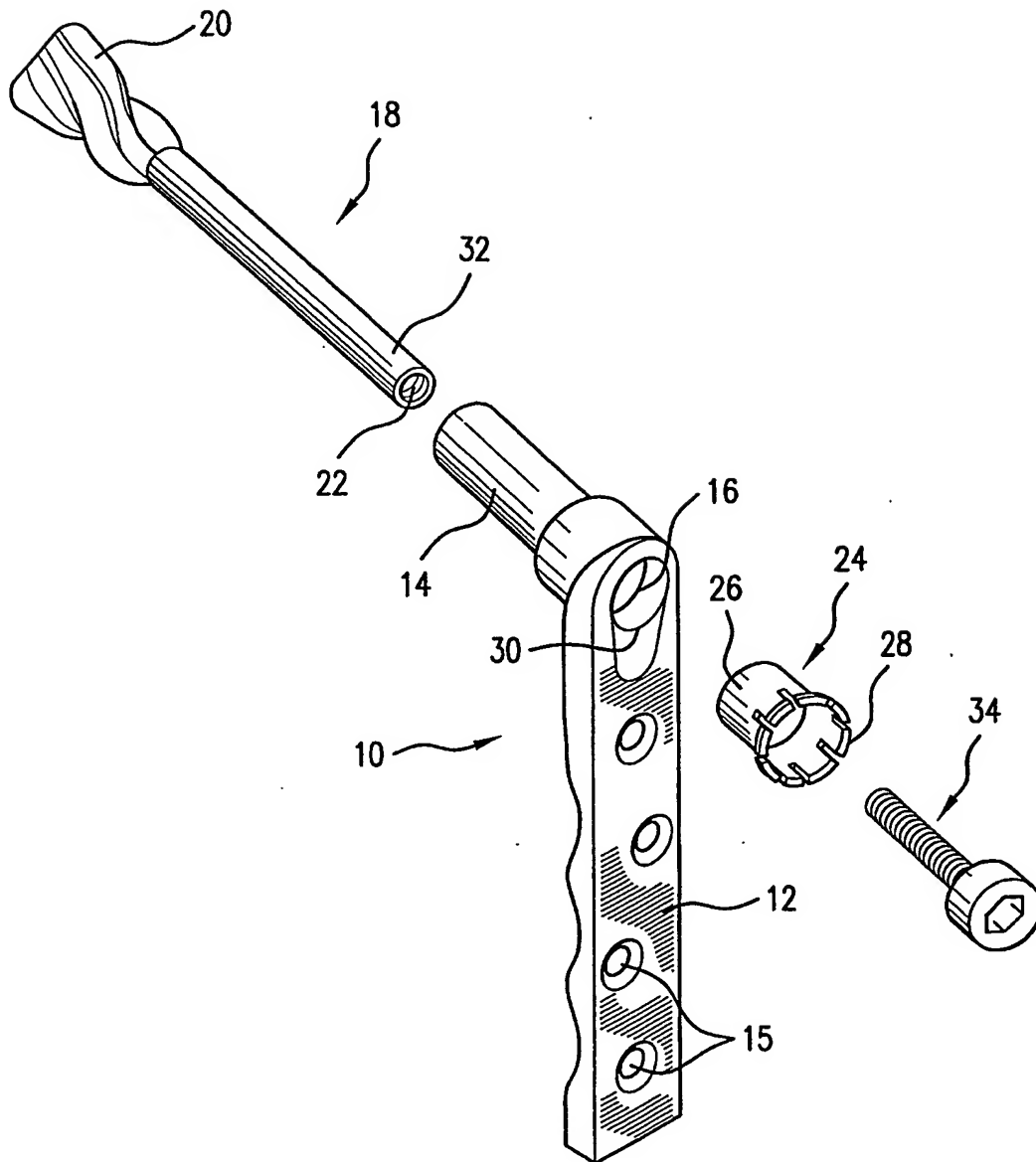


FIG. 1

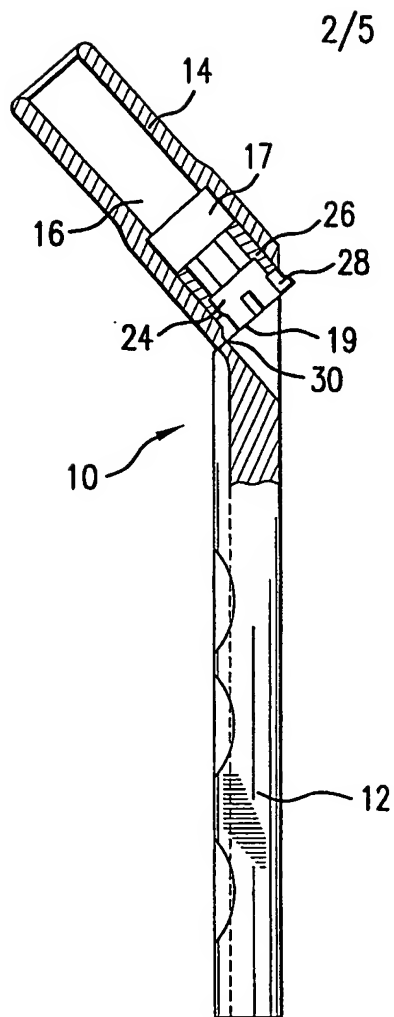


FIG. 2

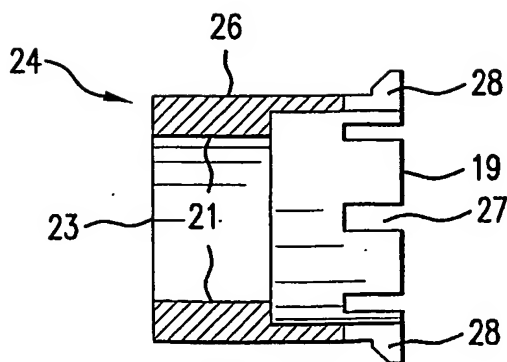


FIG. 3A

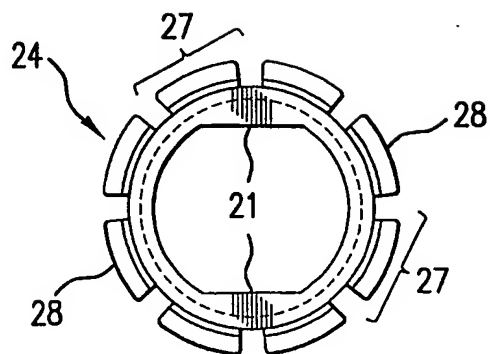


FIG. 3B

3/5

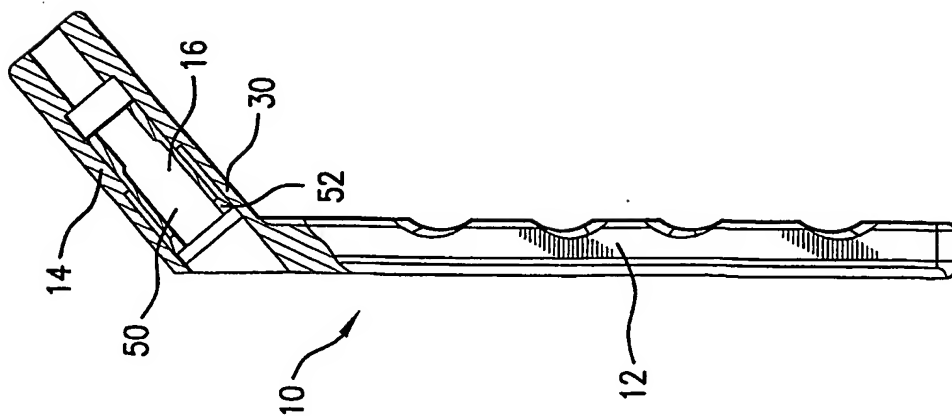


FIG. 4

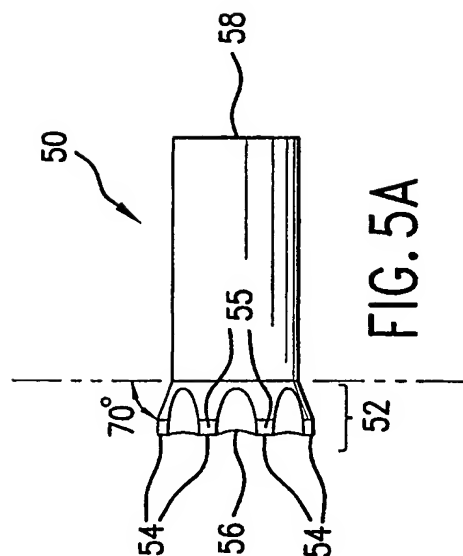


FIG. 5A

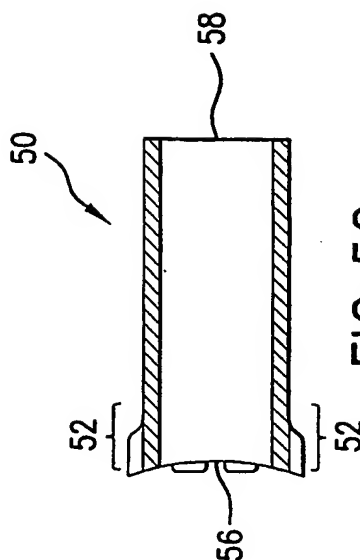


FIG. 5B

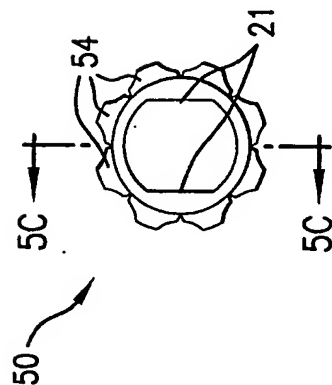


FIG. 5C

4/5

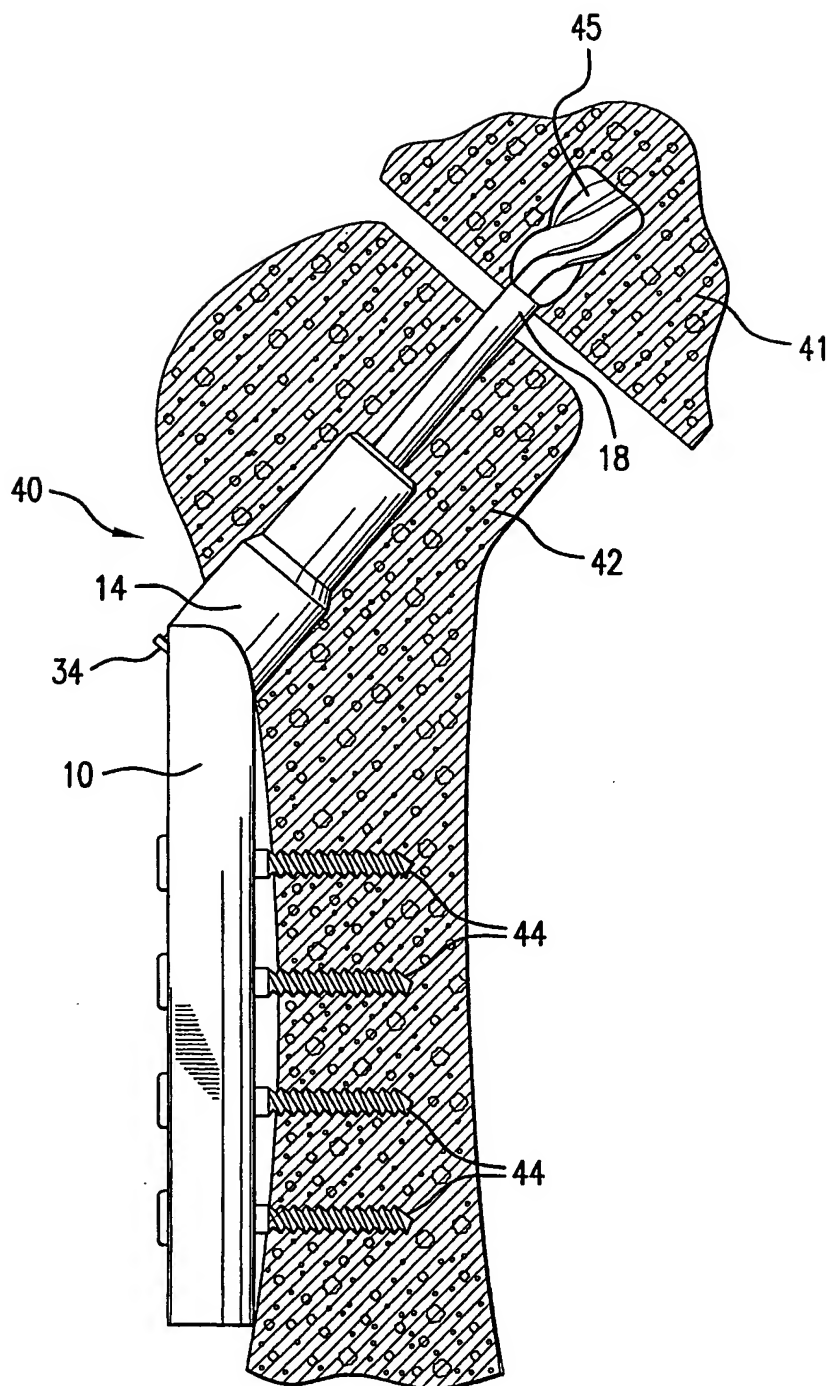


FIG. 6

5/5

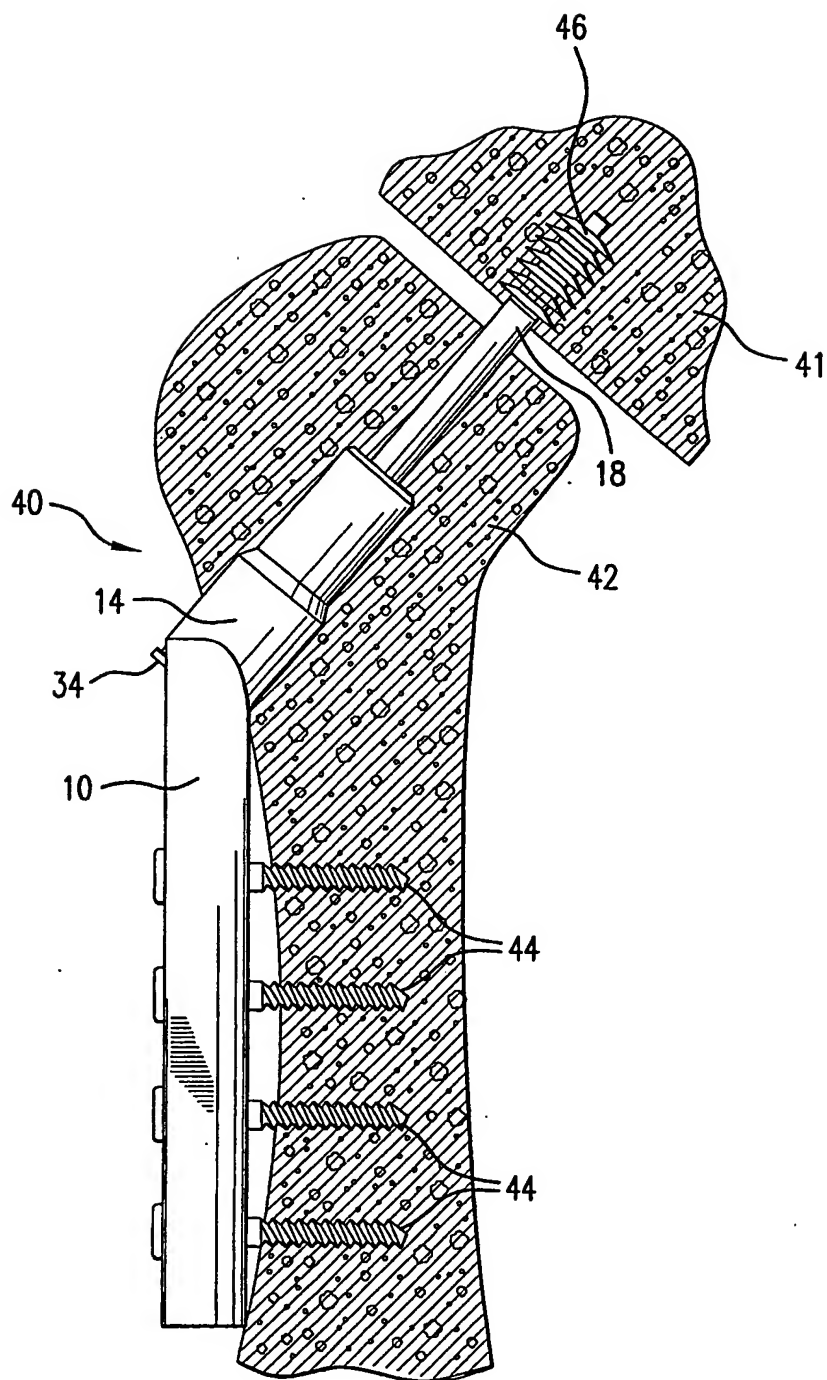


FIG. 7



## INTERNATIONAL SEARCH REPORT

International Application No  
PCT/US 02/30929

**A. CLASSIFICATION OF SUBJECT MATTER**  
IPC 7 A61B17/74

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
IPC 7 A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 530 355 A (GRIGGS CALVIN) 23 July 1985 (1985-07-23) column 3, line 34 - line 40 column 3, line 56 - column 4, line 20 column 5, line 46 - line 58 figures 1-5 -----	1,20

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

## \* Special categories of cited documents:

- \*A\* document defining the general state of the art which is not considered to be of particular relevance
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- \*O\* document referring to an oral disclosure, use, exhibition or other means
- \*P\* document published prior to the international filing date but later than the priority date claimed

- \*T\* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- \*X\* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- \*Y\* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- \*&\* document member of the same patent family

Date of the actual completion of the international search

13 December 2002

Date of mailing of the international search report

07/01/2003

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# INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 02/30929

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 4530355	A	23-07-1985	AT 18984 T 15-04-1986
			DE 3362835 D1 15-05-1986
			EP 0085493 A1 10-08-1983
			US 4617922 A 21-10-1986
			US 4641640 A 10-02-1987
			US 4616638 A 14-10-1986